

ATF R&D STATUS AND PERSPECTIVES

(I3P- THREE PARTIES INSTITUTE CEA-EDF-AREVA)

OECD-NEA Start-up meeting of the Expert Group on
Accident Tolerant Fuels of LWRs
OECD-HQ – Issy les Moulineaux

April, 28-29, 2014

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ATF R&D STATUS IN FRANCE

(no major new technical result since last Oct. 2013 Workshop detailed presentation)

■ **Background - CEA Assets**

More than 30 years of experience on the analytical experimental approach of cladding behavior in LOCA and post-LOCA conditions (EDGAR, DEZIROX, CINOG, ..)

Outcomes of domestic program for innovative fuel claddings and gas cooled reactors

→ Two attractive candidate ATF concepts presented at previous Workshops

■ *Coated Zr-based Cladding → In service, DBA and Post DBA benefits evaluation*

■ *Sandwich SiC-SiC with liner (GFR) → Evaluation of LWR applicability and benefits*

■ **Clad characterizations and evaluation programs are now undertaken with the support of the French Industrial partners AREVA and EDF**

■ **Main 2013 References - Publications:**

[1] J.-C. Brachet, M. Le Flem, C. Sauder, & al., P. Blanpain (Areva-NP) “Status of CEA studies on nuclear fuel claddings for LWRs enhanced accident tolerant fuel: recent results, pending issues and prospects”, proceeding of OECD-NEA ATF Workshop, Oct. 28th, 2013, Issy-les-Moulineaux, France

[2] I. Idarraga et al., “Assessment at CEA of coated nuclear fuel cladding for LWRs with increased margins in LOCA and beyond LOCA conditions”, proceeding of 2013 LWR Fuel Performance Meeting/TopFuel, Charlotte, USA, Sept. 15-19, 2013

[3] C. Sauder et al., “Assessment of SiC/SiC cladding for LWRs”, proceeding of 2013 LWR Fuel Performance Meeting/TopFuel, Charlotte, USA, Sept. 15-19, 2013

COATED ZR BASED CLADINGS

targets :

- Decrease oxidation rate in service and with steam water at high temperature
- Reduce in service hydriding and hydrogen release during accidental sequence
- Improve LOCA behavior (Peak clad T $\searrow$, post quench ductility $\nearrow$)
- Improve long term coolability - procure grace time in the early stage of SA

COATED Zr Alloy

- Experiments made on the most promising coatings
- 1100°C 850 s., **1200°C 300 s.** in steam water + quench
- Weight gain, microstructure observations, Post-quench flexural/tensile tests



First coatings



Improved coatings



Optimized coatings



Weight gain has been decreased
from $\sim 10 \text{ mg/cm}^2$ to $\sim 0,5 \text{ mg/cm}^2$

[Idarraga, Lomello, Billard et al. 2012, unpublished results]

Patents

→ **Optimized Cr coated claddings appears as a candidate for safety improvement in current reactors in a near future**



RECENT RESULTS FOR COATED ZR “SLIGHTLY BEYOND LOCA” CONDITIONS (“BREAKAWAY”... ~4 HOURS AT 1000°C) [1]

	un-coated Zry-4	Non optimized coating	Optimized coating
Weight gain (mg/cm ²)	37-40	11.2	2.5
Zirconia thickness (μm)	~250	0	0
α _{Zr} (O)	~100μm	<100μm + α _{Zr} (O) incursions	0μm + very few α _{Zr} (O) incursions
Hydrogen content (wt.ppm)	~2000-3000	~1000	≤80

For the uncoated Zry-4, the weight gain and the associated hydrogen pick-up are fully consistent with the previous results obtained on low-tin Zry-4 cladding tubes

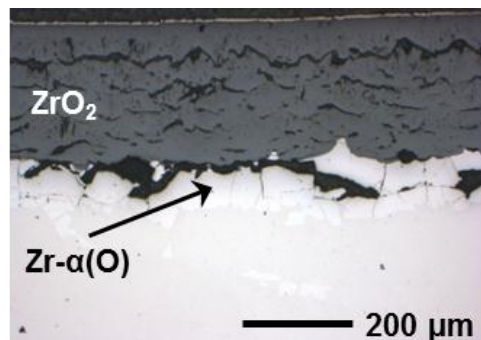
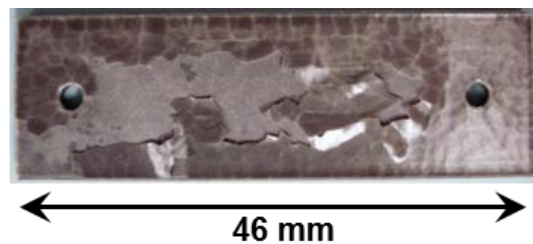
The non-optimized coating induces an intermediate behavior with no significant oxide formation but with some evidence of α_{Zr}(O) incursions into the Zry-4 metallic (prior-β_{Zr}) substrate and an associated significant hydrogen pick-up

The optimized coating exhibits a very good resistance to both oxidation and hydrogen up-take:

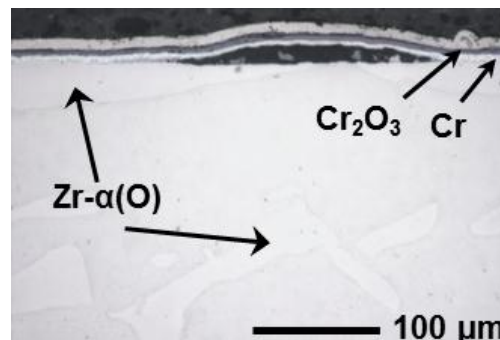
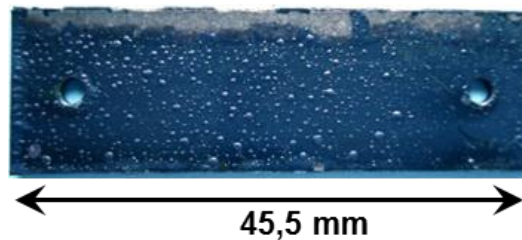
- (i) **absence of significant zirconia formation nor oxygen diffusion into the metallic prior-β_{Zr} substrate**
- (ii) **no significant hydrogen pick-up (<80 wt.ppm).**



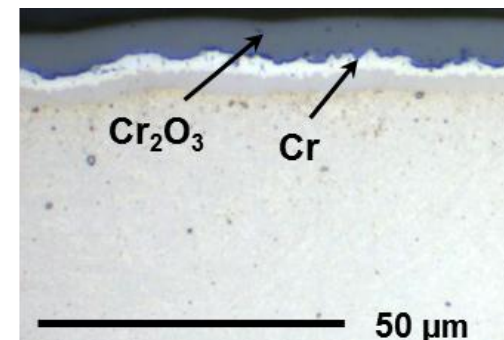
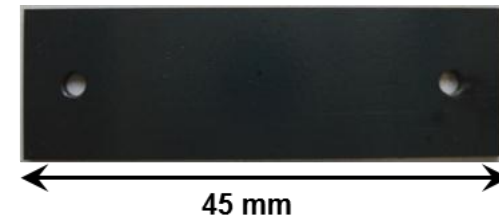
OPTICAL MACRO/MICROGRAPHS OF UNCOATED/COATED ZrY-4 AFTER STEAM OXIDATION FOR 15000 S / 1000°C



Uncoated ZrY-4



Non optimized coating



Optimized coating

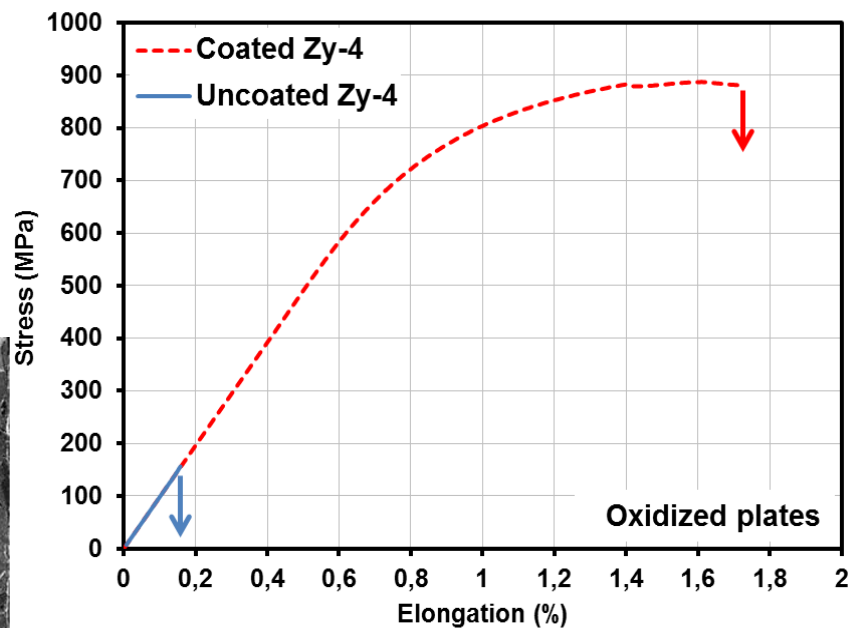
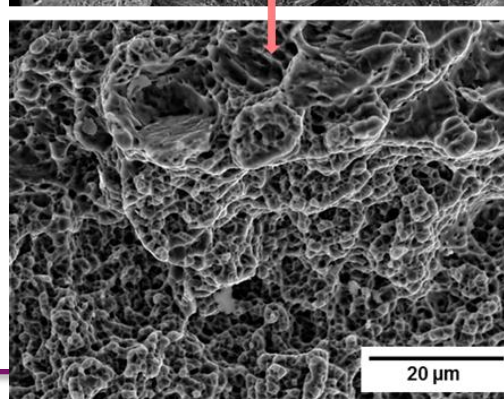
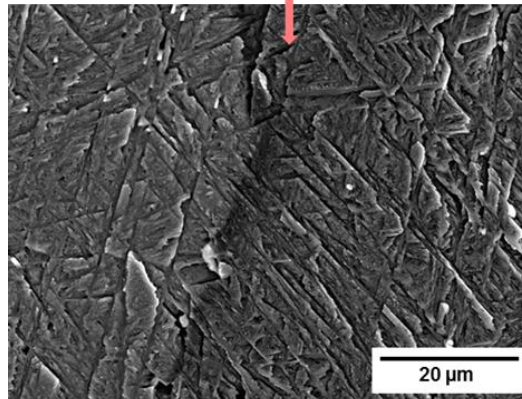
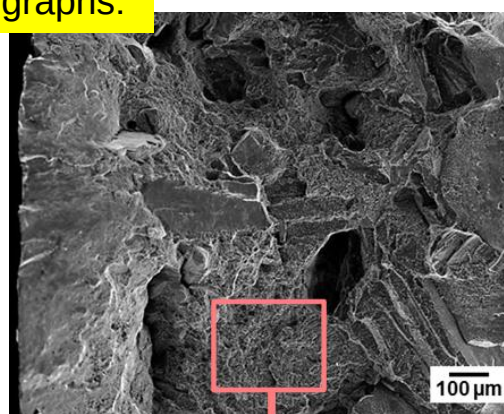
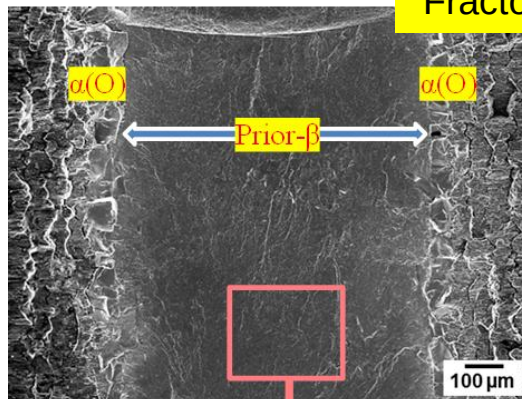
POST-OXIDATION (15000 s AT 1000°C) MECHANICAL TENSILE PROPERTIES

Engineering tensile stress-strain curves obtained at RT on uncoated and optimized coated Zry-4 (after two-side steam oxidation for 15000 s at 1000°C)

Uncoated:

Coated:

Fractographs:

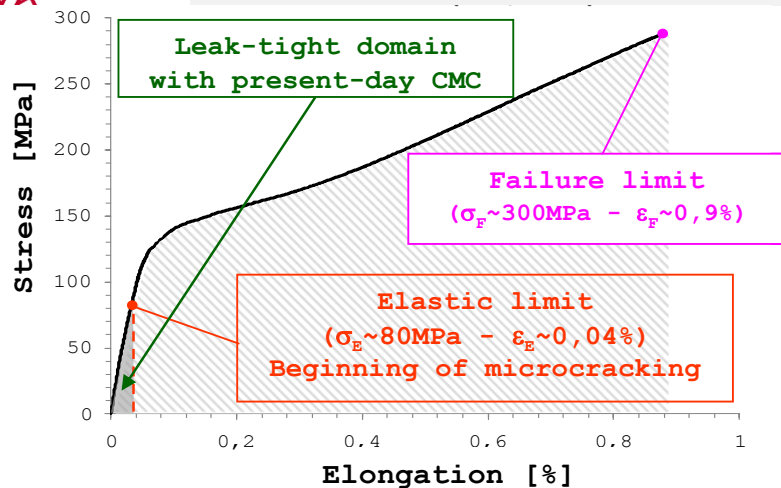


Uncoated Zry-4:

- no significant necking,
 - full brittle failure mode
- Mainly due to the post-breakaway high H content*

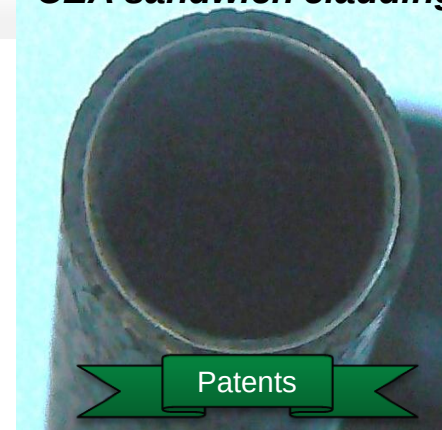
Optimized coated Zry-4:

- significant necking,
 - ductile failure mode (mid-clad-thickness)
- Due to the low oxidation level & [H] <100ppm*



All stages of process are done in CEA

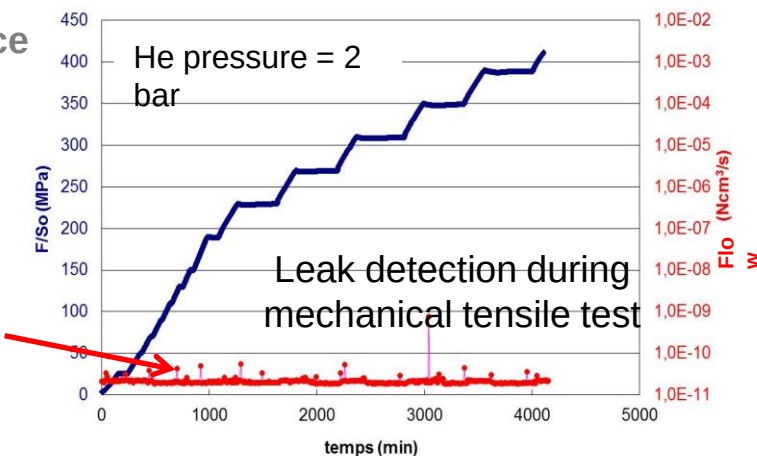
CEA sandwich cladding



Internal tube SiC/SiC:	$e \sim 0.3\text{mm}$
liner Ta :	$e < 0.1\text{mm}$
External tube SiC/SiC:	$e \sim 0.6\text{mm}$

- Metallic layer ensures tightness up to failure limit
- Composite SiC ensures mechanical resistance
- Process is simple and reproducible
- End-plugging solutions (welding)

Leak detection limit



SiC/SiC RESULTS UPDATE AND PROSPECTS [3]

Patents

Oxidation testing (SiC/SiC samples in nominal conditions)

- First oxidation tests of SiC/SiC in LWR nominal conditions for 3500h are promising even if oxidation mechanism must be clearly understood
 - Pyrocarbon interphase is not affected : no reduction of mechanical strength
 - SiC recession is estimated to be 0,5µm after 3500h of LWR nominal oxidation conditions
- Sandwich SiC/SiC cladding must be suitable for LWR

Short/mid term Prospects

- Numerical simulation of rod behavior in Normal operation (PCI, design)
- Fuel-SiC interface issues
- Corrosion /wear in nominal conditions (sandwich concept)
- High temperature oxidation
- Irradiation testing

International collaborations (benchmarking and evaluation)

- SiC-SiC sandwich with Ta liner are candidates to experimental comparisons and numerical approach evaluations

ATF R&D PERSPECTIVES IN FRANCE

Realistic approach based on 3 axes

■ **Material development and innovation (CEA + U collaborations, GFR)**

- Long length tubes (~0,5 m at pilot lab scale) (coated Zr)
- Tight ends for sandwich SiC-SiC concept

Patents

■ **Three Parties Institute (CEA-EDF-AREVA partnership)**

- Characterization testing, experiments and numerical simulation approach of key properties for thermo-mechanical design such as corrosion, erosion, LOCA behavior, irradiation evaluation (small samples at marginal cost in domestic sample holder)
- Specific roadmap under construction for each concept

■ **Involvement in International programs**

- Participation to OECD/AEN Workshop and Expert Group
- Proposal of Zy-4 coated UO₂ fuel rodlets for irradiation in the Halden Reactor Program
 - Step 1 : Assessment of coating stability in service condition (PCI design possible)
 - Step 2 : Evaluation of Benefits in LOCA Transient
- Proposal in the framework of Nugenia WP5 (EDF « RAMAT » proposal to be discussed with other ones for unified proposal in H2020 call for tender)

PROPOSALS FOR EXPERT GROUP ACTIVITIES EXPECTATIONS / CONTRIBUTION

Expectations from EG

■ Guidelines for ATF candidate evaluation

- Definition of « safety benefit », how to « measure » it
- Choice of scenarii
 - Normal operation → DBA → early stages of post DBA → Severe Accident
 - For each stage reduction of probability /consequence is a benefit

Proposals for EG activities

■ Parametric approach by variation of some key properties

- On the base of scenarii selected by EG
- Using system codes (MAAP, MELCOR, ASTEC, ...)
- Change one (or a set of) property(ies) considered as Key (T melt / Thermal conductivity, oxydation kinetics , oxidation reaction enthalpy,..
- Evaluate the « safety benefit » of this change for the selected scenarii

■ Exchange of basic properties related to ATF material candidates

- Cross benefit evaluations (-/- scenarii)

■ Main output of EG

- Safety benefit evaluation guide
- Scenarii
- Tools for prioritization of development Map (difficulty, expected benefit)

SYNERGIES WITH OTHER INTL PROGRAMS

OECD-NEA Halden Reactor Project (WGFS)

- Proposal for irradiation testing of Cr-coated- Zy-4/UO₂ – fuel rodlets (White paper submitted)

- Goals

Step 1

- Direct evaluation of under representative PWR conditions
- Stability of the protective effect of coating
 - In environment
 - In environment + local deformation (special design for early contact)
- Conditioning irradiated rodlet(s) for LOCA test in a second step

Step 2

- LOCA test – Direct benefit evaluation

- Timing

15 - 20 cm length clads may be short term delivered now

50 - 60 cm clads could be fabricated end 2014 / early 2015

Discussion on detailed program and PIE expected around mid-2014

NUGENIA Technical Area 5 :

- several proposals to be coordinated around ATF cross evaluation goals and basic data acquisition (Falstaff, Forclad, Ramat, ...) → Call H2020 in 2014/9
- need of harmonization with other ATF initiatives